

Characterization of a super hydrophobic soot-coated glass insulator

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Abstract— Deal with electrical flashovers problems, insulating materials with superhydrophobic surface are ideal for manufacturing insulator systems to improve their performances. This paper deals with the electrical aging phenomenon effect on the hydrophilic and superhydrophobic surface of glass insulators in service. At this purpose, a physicochemical experimental study of glass (G) and soot-coated glass (SCG) insulators electrically aged under wet conductive pollution is undertaken. At first, accelerated electrical degradation tests were conducted under a growing alternating 50 Hz homogeneous electrical field on glass and soot-coated glass samples. A series of surfacic breakdown is carried out on these two materials in both clean and polluted surfaces to characterize their performances. The measurements of the contact angle, the dielectric strength, the capacitor and the loss factor are performed on virgin (Vg) and electrically aged (EA) samples in the two surface states; clean (C) and polluted (P). This latter case is performed using wet conductive pollutant with electrical conductivity of 2 mS/cm² and 5 mS/cm². Then series of chemical analyses, as a light microscopy (LM) analysis, an Infrared spectroscopy FTIR and X-ray diffraction analysis (XRD) were performed to monitor the degradation at microscopic scale. Electrical and chemical measurements have evidenced the constraints effects on the G and SCG aging phenomenon, and a correlation between the different results was established.

Keywords— Aging, light microscopy, Infrared spectroscopy, X-ray diffraction analysis, Pollution, Soot-coated glass.

I. INTRODUCTION

Flashover phenomena compromise electrical energy transmission and high-voltage infrastructure durability [1], [2]. Natural and industrial contaminants aggravate this issue, particularly under elevated humidity conditions [3]-[6]. This is because humidification of the pollution layer triggers insulator flashover, disrupting transmission networks. Indeed, when subjected to an electric field, a water droplet accumulated on the external insulator surface can deform, generating an intense localized field that disrupts the surrounding environment. This can trigger partial discharges, which may escalate into an electric arc, ultimately leading to insulator flashover [7], [8]. Utilizing hydrophobic and superhydrophobic materials offers a viable solution to this issue, as they effectively reduce leakage currents and decrease the likelihood of dry band formation, thereby enhancing insulation performance in polluted environments [9]-[12].

This study focuses on the physicochemical analysis of electrically aged glass (G) and soot-coated glass (SCG) insulators. It aims to assess the contact angle (θ), dielectric strength (E_l), capacitance (C_x), and loss factor ($tg\delta$) before and after aging, both with and without pollution effects. The material's behavior at the molecular level is examined through chemical analyses, including Light Microscopy LM analysis, FTIR infrared spectroscopy and XRD X-ray diffraction, to characterize the impact of electrical degradation under polluted conditions on its microstructure.

II. EXPERIMENT

The investigations are carried out on parallelepiped G and SCG film samples $100 \times 100 \times 5$ mm³ in dimensions. The accelerated electrical degradation tests are performed under increasing uniform field, under AC - 50 Hz voltage ramp with speed of 2kV_{max}/s. A series of 100 surface flashover is carried out with a plane-plane electrode geometry (fig.1). Polluted (P) and clean (C) G and SCG surface conditions are considered. The pollutant used is a sodium chloride solution (NaCl) with two electrical conductivities namely, $\sigma = 5$ mS/cm² and $\sigma = 2$ mS/cm², noted (2) and (5) respectively. Series of physical and electrical measurements and chemical analyses are conducted on virgin in clean surface (VgC), virgin in polluted surface (VgP), electrically aged in clean surface (EAC) and electrically aged in polluted surface (EAP) conditions G and SCG samples. Contact angle (θ), longitudinal dielectric strength (E_l), capacitance (C_x) and loss factor ($tg\delta$)

measurements are undertaken. θ is determined in the horizontal plane of the glass plate surface, for a droplet volume $V=4\mu\text{l}$ (fig. 2). C_x and $\text{tg}\delta$ are measured under a voltage levels $V_{rms} = 100\text{ V}$ at increasing frequencies ($f = 100\text{ Hz}$ to 1100 Hz in increasing steps from 10 to 100 Hz) using Schering bridge. To monitor the degradation at microscopic scale, the following analyses are conducted: LM is performed with a magnification of 400 and 1000. It allows to relevantly seeing the changes occurred on the relief material. FTIR is carried out by subjecting the samples to electromagnetic radiation in the infrared wavelength range of $2.5\text{ }\mu\text{m} < \lambda < 50\text{ }\mu\text{m}$. Samples are exposed to XRD with a wavelength beam ($0.1\text{ nm} < \lambda < 10\text{ nm}$).

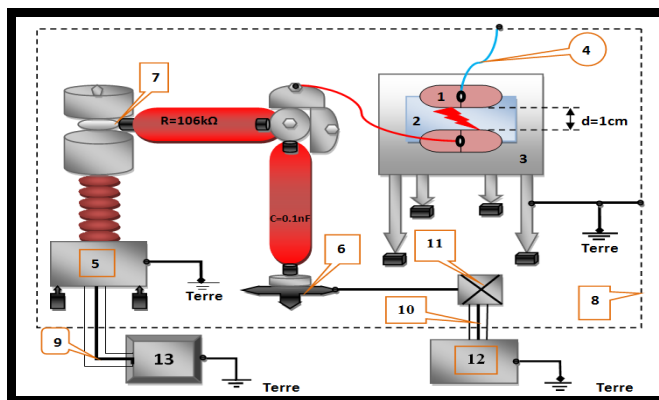
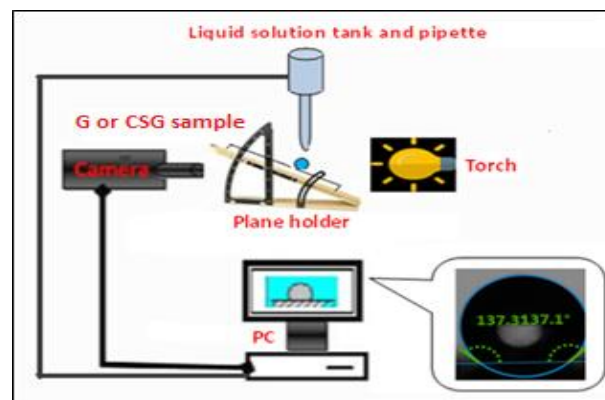


Fig. 1 Experimental device of electrical aging

Fig. 2 Experimental setup of contact angle θ measurement

Where, 1: Copper electrode, 2: Solid materials (G or CSG), 3: Table, 4: Wire, 5: High voltage transformer, 6: Element support, 7: Connection nodes, 8: Protection grid, 9 and 10: Coaxial cable, 11: Connection box, 12: MU11 Peak Voltmeter, 13: SG1BT manual and automatic control system.

III. EXPERIMENTAL RESULTS

A. Aging and Pollution Effects on G and SCG Electrical Performance

The electrical aging affects both G and SCG longitudinal dielectric strength (Table I). This quantity decreases under the effect of electrical stress. The soot coating increases the surface conductivity of the glass, further degrading its dielectric strength. In the presence of conductive pollution deposits, this reduction worsens. And it is even more marked when the conductivity of the polluting layer is increased (Fig. 3). The work of the authors [13] and [14] has a slight approach with those presented above relating to the G insulator. G and SCG electrical aging leads to a reduction of C_x , which decreases more significantly with higher voltage frequency (Fig. 4). The decline in this value indicates material deterioration, which is more significant in the presence of pollution. A slight approach to G results can be made with those of [15]. The G loss factor $\text{tg}\delta$ decreases as the frequency of the excitation (or measurement) signal increases. This result implies that the material responds in frequency like an equivalent circuit with localized parallel RC constants, making it well-suited for high-frequency operation due to its superior energy quality efficiency. The electrical aging leads to an increase in the loss factor, which becomes more pronounced with the rise in conductivity of the polluted layer. $\text{Tg}\delta$ is more important in the EAP case compared to the EAC and Vg one (Fig. 5). A slight approach to G results can be made with those of [15].

TABLE I

LONGITUDINAL DIELECTRIC STRENGTH EL

State	Longitudinal dielectric strength El (kV/cm)			
	VgC	VgP		EAC
		wet pollution $\sigma=2 \text{ mS/cm}^2$ $\sigma=5 \text{ mS/cm}^2$		EAP wet pollution $\sigma=2 \text{ mS/cm}^2$ $\sigma=5 \text{ mS/cm}^2$
G	a	15.26		
	b			14.04
	c	12.86		
	d		11.58	
	e			10.54
	f			8.4
SCG	g	13.2		
	h		12.12	
	i	11.34		
	j		9.5	
	k			9.40
	l			7.36

Where: for G (a: VgC, b: EAC, c: VgP at $\sigma=2 \text{ mS/cm}^2$, d: VgP at $\sigma=5 \text{ mS/cm}^2$, e: EAP at $\sigma=2 \text{ mS/cm}^2$ and f: EAP at $\sigma=5 \text{ mS/cm}^2$), and for SCG (g: VgC, h: EAC, i: VgP at $\sigma=2 \text{ mS/cm}^2$, j: VgP at $\sigma=5 \text{ mS/cm}^2$, k: EAP at $\sigma=2 \text{ mS/cm}^2$ and l: EAP at $\sigma=5 \text{ mS/cm}^2$).

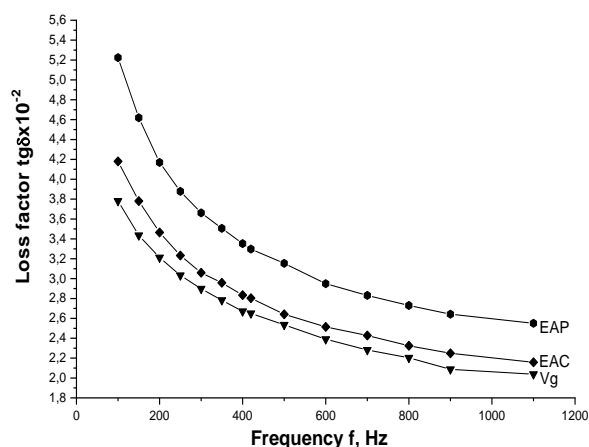


Fig. 4 Cx versus frequency for different G states: virgin, aged in clean and polluted conditions

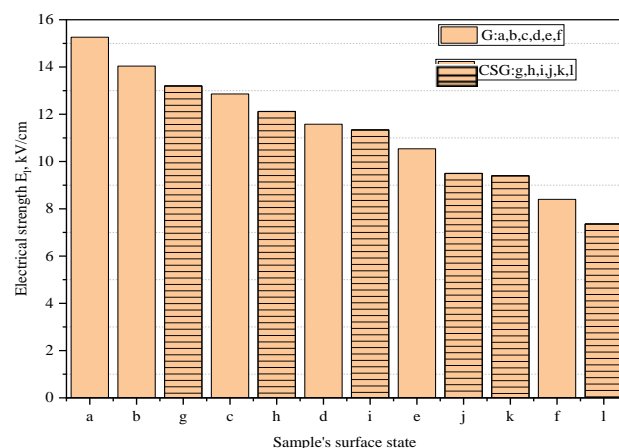


Fig. 3 El Histogram versus G and SCG surface condition

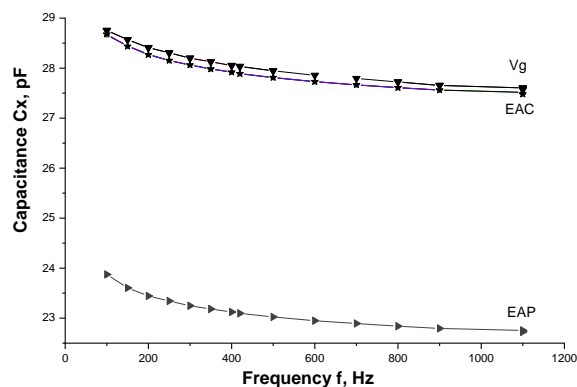


Fig. 5 $\text{tg } \delta$ versus frequency depending on G states: virgin, aged in clean and polluted conditions

B. Aging and Pollution Effects on G and SCG hydrophilic and superhydrophobic Performance

In its youthful state (VgC), G is hydrophilic (figs. 6 and 7.A) [16]. Its aging (EAC) caused by multiple flashover and imposed pollution conditions (EAP2 and EAP5) at $\sigma=2 \text{ mS/cm}^2$ and $\sigma=5 \text{ mS/cm}^2$ respectively, leads to an attenuation of this characteristic, which is however less pronounced in the case of severe pollution, which damages its surface without making it hydrophobic (fig. 6). Conversely, SCG is superhydrophobic in its youth (VgC) (figs. 6 and 7.B), and its aging partially affects this characteristic (EAC), especially in the presence of wet pollution (EAP). This last point agrees with the results of [16] carried out on G insulator. However, severe pollution intensifies the discharge which sweeps away soot in its path, and the dust cloud formed strengthens its peaks, which compensates for this loss and allows the material to regain its superhydrophobic characteristic (fig. 6).

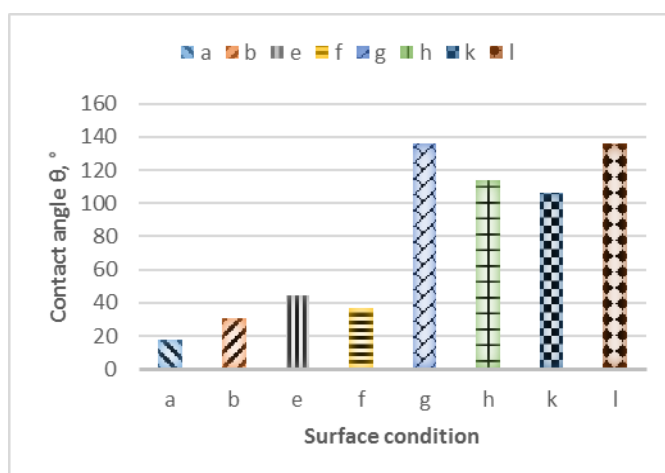
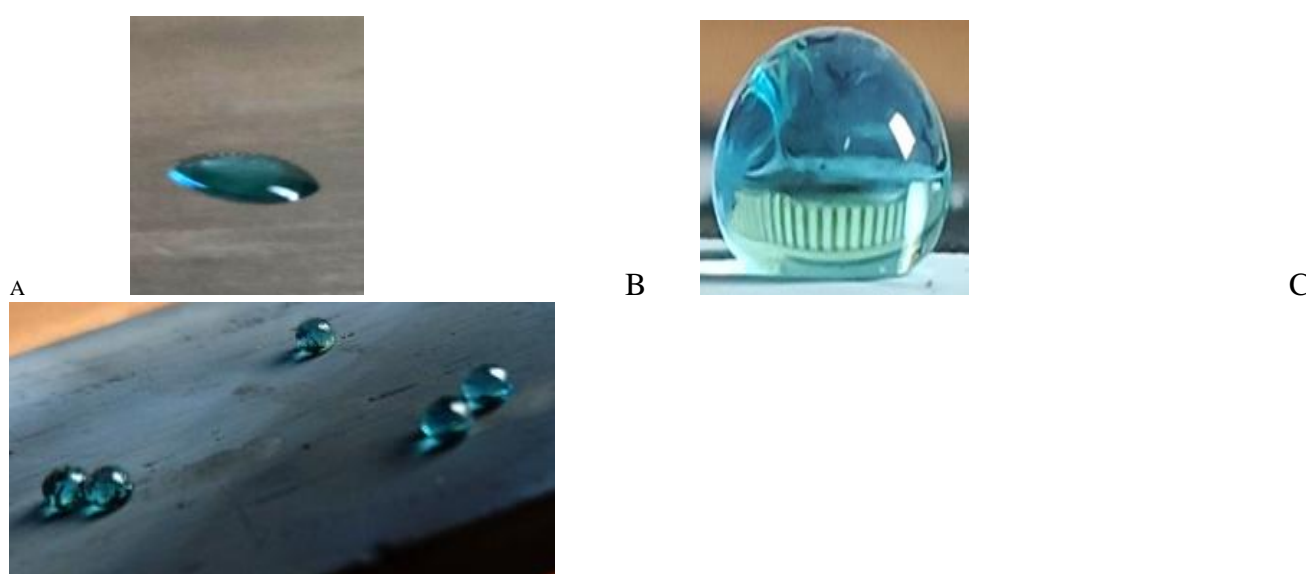
Fig. 6 θ Histogram versus G and SCG surface condition

Fig. 7 Water droplet on: A) hydrophilic G and B) and C) superhydrophobic SCG surface

C. Aging and Pollution Effects on G and SCG Surface Morphology

The observations and photographic shoot made with LM analysis of G and SCG samples aged under electric field stress in the clean and polluted state revealed traces left by the discharge. The latter caused a carbonization and a surface depolishing of G sample, which becomes rough, giving it a quasi-hydrophobic character (fig. 6, 8.B and 8.C), unlike the superhydrophobic character of the SCG sample, which is affected. However, its aging under severe pollution at $\sigma = 5 \text{ mS/cm}^2$ promotes the electrical arcing initiation following the establishment of a leakage current through the superficial layer; This reveals, over the entire surface, sinuous traces of the tree-like discharge that sweeps away soot in its path, thus promoting the formation of peaks. This gives the surface a rough appearance which improves its superhydrophobic character (fig. 6, 7.B and 8.D).



A. VgC-G (a) sample

B. EAC-G (b) sample

C. EAP5-G (f) sample

D. EAP5-SCG (l) sample

Figure 8. LM photographic of G and SCG samples

D. *Aging and Pollution Effects on G and SCG Molecular Structure*

FTIR analysis revealed two distinct regions: the first region starting from 4000 to 1500 cm^{-1} related to hydroxyl groups (O-H) and groups linked to bonds (C-H and C-O, C=O, C=C); the second region, ranging from 1600 to 400 cm^{-1} ; related to the compound's fingerprint and the different groups characterizing structural bonds generally linked to glass (Si-O, Al-O, etc.) (fig.9). Thus, very broad bands located between 991 and 1021 cm^{-1} are observed; they are attributed to the Si-O bond related to glass. However, pollution caused two broad bands to appear at 3430 and 1670 cm^{-1} for samples e (G-EAP2) and f (G-EAP5); these are attributed to the presence of external hydroxyl groups of O-H characterizing H-O-H bonds.

The application of soot on glass revealed several bands characterizing the bonds of the organic compounds making up the soot; furthermore, the influence of aging and pollution on the soot associated with the glass is revealed by the pronounced presence of new vibration bands.

The spectra of samples g (SCG-VgC), h (SCG-EAC), k (SCG-EAP2) and l (SCG-EAP5) show the presence of peaks characterizing the functional groups at 2962 , 2932 and 2859 cm^{-1} for CH₂ and CH₃ bonds respectively; related to the aliphatic cycles of soot. These peaks are much more intense when the samples are not subjected to pollution (samples g and h). On the other hand, as pollution increases, broad bands appear around 3430 cm^{-1} which are attributed to the presence of external OH indicating the presence of water (H-O-H).

In the spectrum (1600 - 500 cm^{-1}), several intense bands appear, attributed to the different aromatic cycles making up the soot. The bands noted at 1470 cm^{-1} are attributed to the functional groups of the C-H bonds of the aliphatic cycles CH₂ and CH₃, these peaks become much more intense as pollution increases.

On the other hand, a broad band at 1650 cm^{-1} is observed, attributed to the presence of aromatic cycles C-C, C-H, and C-O-C. The structure of the glass is greatly influenced by the presence of soot and pollution, which is noted by the presence and broadening of the peaks at 991 cm^{-1} , related to the Si-O bond.

The X-ray spectra recorded in 2θ between 5° and 80° show the almost complete absence of crystalline phases, which indicates that the glasses have a totally amorphous structure, noted by the hump that exists between $20 - 25 [^\circ 2\theta]$. However, some peaks appear between ($27.47 - 36.13$ and 54.38) $[^\circ 2\theta]$ characteristic of rutile and a crystalline phase of Chromium Manganese Telluride which diffracts at (28.40 and 29.49) $[^\circ 2\theta]$. Note, however, the shift towards small angles of the XRD spectrum of sample h (SCG-EAC) relative to samples a (G-VgC) and b (G-EAC), as well as the disappearance of the hump at angle $12 [^\circ 2\theta]$ of sample l (SCG-EAP5) relative to samples f (G-EAP5) and g (SCG-VgC). This suggests that electrical aging and

pollution have effects on the structure of the soot or the soot-glass interaction. The pollutant could have an impact on the charge distribution at the glass surface and modify the interaction between the soot and the glass. The changes in surface morphology observed in ML suggest that the pollutant (NaCl) could modify the soot structure, making it more compact or uniform, create nucleation sites for deposit growth, and influence the mobility of species on the glass surface, which would explain the loss of the hump in the XRD spectrum, as the soot structure is modified.

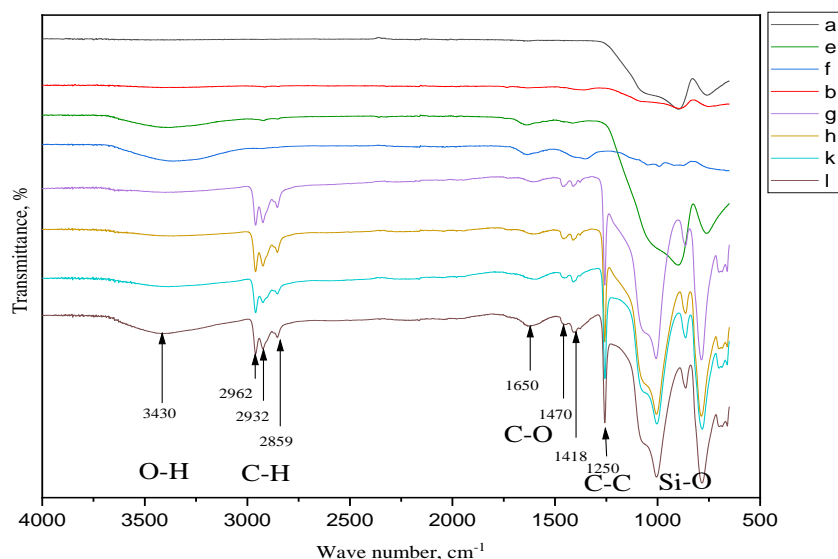


Fig. 9 FTIR spectra of G and SCG samples (virgin and aged, polluted at $\sigma=2\text{mS/cm}^2$ and at $\sigma=5\text{mS/cm}^2$)

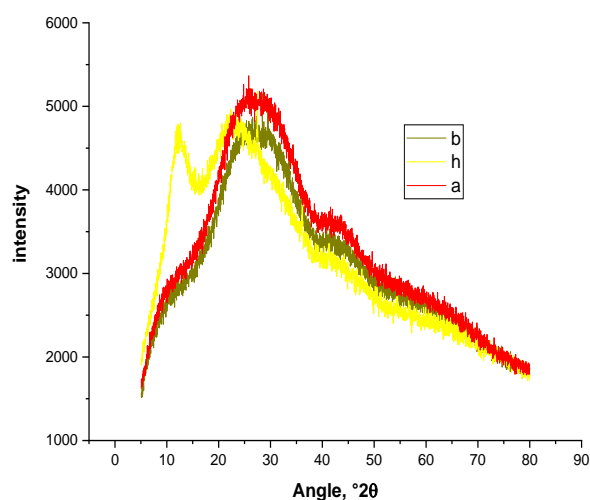


Fig. 10 X-ray diffractogram of different glass samples: a (G-VgC), b (G-EAC) and h (SCG-EAC)

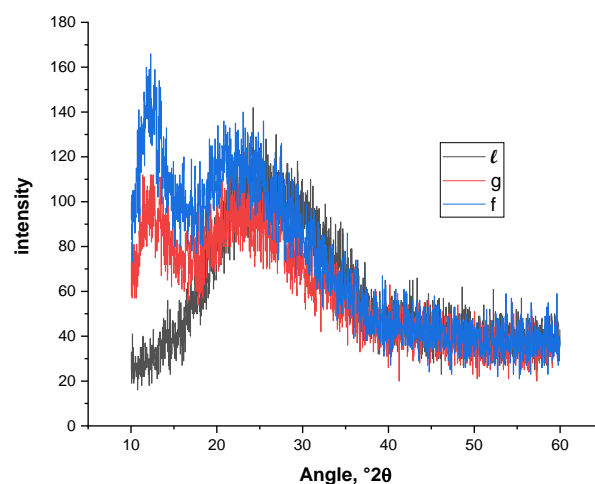


Fig. 11 X-ray diffractogram of different glass samples: f (G-EAP5), g (SCG-VgC) and l (SCG-EAP5)

IV.CONCLUSION

The results of electrical and physical measurements, supported by a light microscopy (LM), X-ray diffraction (XRD) and Infrared spectroscopy (FTIR) analyses, showed that the glass structure is highly influenced by aging and the presence of soot and pollution, and that electrical aging under severe pollution conditions (conductivity $\sigma=5\text{ mS/cm}^2$) degrades the electrical properties of the glass (dielectric strength E_i , electrical loss factor $\text{tg}\delta$, capacitance C_x).

This is revealed by FTIR analyses highlighting the presence of peaks characterizing the functional groups of CH₂ and CH₃ bonds related to the aliphatic cycles of soot, and the appearance of several intense bands attributed to the various aromatic cycles composing the soot C-C, C-H, and C-O-C, as well as by the

broadening of peaks related to the Si-O bond. Similarly, LM and XRD analyses revealed the electrical aging and pollution effects on the structure of the soot and the soot-glass interaction. XRD lets suggest that the pollutant could have an impact on the charge distribution at the glass surface and modify the interaction between the soot and the glass. Likewise, LM analysis revealed changes in surface morphology related to the NaCl pollutant which could modify the soot structure, making it more compact or uniform, create nucleation sites for deposit growth, and influence the mobility of species on the glass surface.

Thus, the glass degradation under the applied field stress and the presence of soot and pollution can be directly linked to the embrittlement of this material following the phase change, the oxidation mechanism produced, and the alteration of its surface under the effect of intense discharge energy, which results in a decrease in its electrical and physical performance. The polar nature of the conductive pollutant solution (NaCl) contributes to this degradation.

In contrast, the application of electrical field stress, combined with the presence of severe pollution, improves the hydrophobic, or even superhydrophobic, character of its surface by making it rough; this lowers the surface energy and makes the contact area between the solid (glass) and the fluid (droplets) negligible. This can be explained by the nano- and micro-structured arrangement produced by the discharge, and by the large amount of air that is trapped in the topography, which makes the friction between water and air, and air and air almost zero [17].

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